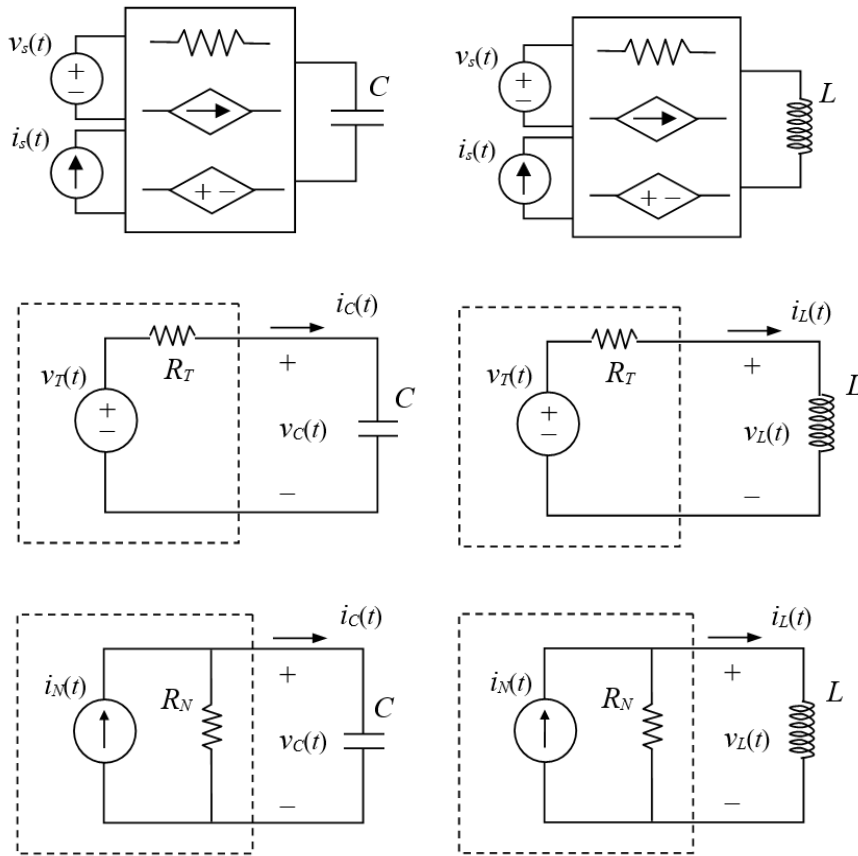


Chap 3 First-Order Linear Circuits



3.1 Laplace Transform

- Laplace transform of $f(t)$, $t \geq 0$

$$(3.1-1) \quad \mathcal{L}\{f(t)\} = \int_0^{\infty} f(t)e^{-st} dt \quad \text{or} \quad \hat{f}(s) = \int_0^{\infty} f(t)e^{-st} dt$$

- Laplace transform of $f'(t)$, $t \geq 0$

$$(3.1-2) \quad \mathcal{L}\{f'(t)\} = s\hat{f}(s) - f(0)$$

Prove:
$$\mathcal{L}\{f'(t)\} = \int_0^{\infty} f'(t)e^{-st} dt = \int_{t=0}^{\infty} e^{-st} df(t) = e^{-st} f(t) \Big|_0^{\infty} - \int_{t=0}^{\infty} f(t) de^{-st}$$

$$= e^{-s\infty} f(\infty) - f(0) + s \int_{t=0}^{\infty} f(t)e^{-st} dt$$

If $Re(s) > 0$, we have $e^{-s\infty} f(\infty) = 0$ and thus

$$\mathcal{L}\{f'(t)\} = -f(0) + s \int_{t=0}^{\infty} f(t)e^{-st} dt = s\hat{f}(s) - f(0)$$

- Laplace transform of $\int_0^t f(\tau) d\tau, t \geq 0$

$$(3.1-3) \quad \mathcal{L}\left\{\int_0^t f(\tau) d\tau\right\} = \frac{1}{s} \hat{f}(s)$$

Prove: Let $g(t) = \int_0^t f(\tau) d\tau$, then $g(0) = 0$ and $g'(t) = f(t)$.

From (3.1-7), we have $\mathcal{L}\{g'(t)\} = s\mathcal{L}\{g(t)\} - g(0) = s\mathcal{L}\{g(t)\}$

$$\text{i.e., } \mathcal{L}\{g(t)\} = \frac{1}{s} \mathcal{L}\{g'(t)\} \text{ or } \mathcal{L}\left\{\int_0^t f(\tau) d\tau\right\} = \frac{1}{s} \mathcal{L}\{f(t)\} = \frac{1}{s} \hat{f}(s)$$

- Laplace transform of $e^{-at} f(t), t \geq 0$

$$(3.1-4) \quad \mathcal{L}\{e^{-at} f(t)\} = \int_0^\infty e^{-at} f(t) e^{-st} dt = \int_0^\infty f(t) e^{-(s+a)t} dt = \hat{f}(s+a)$$

- $\mathcal{L}\{f(t)\}$ for $f(t) = 1, t, e^{-at}, e^{j\omega t}, t \geq 0$.

$$(3.1-5) \quad \mathcal{L}\{1\} = \int_0^\infty 1 \cdot e^{-st} dt = -\frac{1}{s} \int_0^\infty de^{-st} = -\frac{1}{s} e^{-st} \Big|_{t=0}^\infty = \frac{1}{s}$$

$$(3.1-6) \quad \mathcal{L}\{t\} = \int_0^\infty t \cdot e^{-st} dt = -\frac{1}{s} \int_0^\infty t \cdot de^{-st} = -\frac{1}{s} \left(te^{-st} \Big|_0^\infty - \int_0^\infty e^{-st} dt \right) = \frac{1}{s^2}$$

$$(3.1-7) \quad \mathcal{L}\{e^{-at}\} = \int_0^\infty e^{-at} e^{-st} dt = \int_0^\infty e^{-(s+a)t} dt = \frac{1}{s+a}$$

$$(3.1-8) \quad \mathcal{L}\{e^{j\omega t}\} = \int_0^\infty e^{j\omega t} e^{-st} dt = \frac{1}{s - j\omega} = \frac{s}{s^2 + \omega^2} + j \frac{\omega}{s^2 + \omega^2}$$

- Since $\mathcal{L}\{e^{j\omega t}\} = \mathcal{L}\{\cos \omega t + j \sin \omega t\}$ and $\mathcal{L}\{e^{-at} f(t)\} = \hat{f}(s+a)$, we have

$$(3.1-9) \quad \mathcal{L}\{\cos \omega t\} = \text{Re}\left(\mathcal{L}\{e^{j\omega t}\}\right) = \frac{s}{s^2 + \omega^2}$$

$$(3.1-10) \quad \mathcal{L}\{\sin \omega t\} = \text{Im}\left(\mathcal{L}\{e^{j\omega t}\}\right) = \frac{\omega}{s^2 + \omega^2}$$

$$(3.1-11) \quad \mathcal{L}\{te^{-at}\} = \frac{1}{(s+a)^2}$$

$$(3.1-12) \quad \mathcal{L}\{e^{-at} \cos \omega t\} = \frac{s+a}{(s+a)^2 + \omega^2}$$

$$(3.1-13) \quad \mathcal{L}\{e^{-at} \sin \omega t\} = \frac{\omega}{(s+a)^2 + \omega^2}$$

3.2 RC Circuit

- Capacitor model with initial voltage $v_C(0) = v_{C0}$

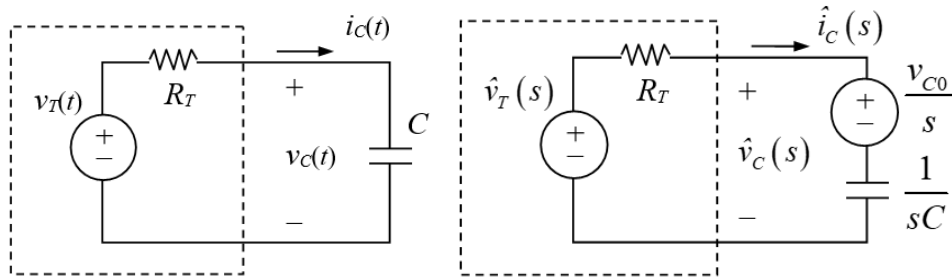
$$(3.2-1) \quad v_C(t) = v_{C0} + \frac{1}{C} \int_0^t i_C(\tau) d\tau$$

$$(3.2-2) \quad \hat{v}_C(s) = \frac{v_{C0}}{s} + \frac{1}{C} \left(\frac{\hat{i}_C(s)}{s} \right) \Rightarrow \hat{v}_C(s) = \frac{v_{C0}}{s} + \frac{1}{sC} \hat{i}_C(s)$$

$z_C(s)$

$$z_C(s) = \frac{1}{sC} : \text{impedance of capacitor.}$$

3.2.1 RC Circuit with Voltage Source



- Mathematic model

$$(3.2.1-1) \quad \hat{v}_T(s) = R_T \hat{i}_C(s) + \frac{v_{C0}}{s} + \frac{1}{sC} \hat{i}_C(s) = \left(R_T + \frac{1}{sC} \right) \hat{i}_C(s) + \frac{v_{C0}}{s}$$

$$\Rightarrow \hat{i}_C(s) = \left(R_T + \frac{1}{sC} \right)^{-1} \left(\hat{v}_T(s) - \frac{v_{C0}}{s} \right) = \frac{sC}{1 + sR_T C} \hat{v}_T(s) - \frac{Cv_{C0}}{1 + sR_T C}$$

$$\Rightarrow \hat{v}_C(s) = \frac{v_{C0}}{s} + \frac{1}{sC} \hat{i}_C(s) = \frac{v_{C0}}{s+a} + \frac{a}{s+a} \hat{v}_T(s), \quad a = \frac{1}{R_T C} > 0$$

$$\Rightarrow v_C(t) = \mathcal{L}^{-1} \left\{ \frac{v_{C0}}{s+a} \right\} + \mathcal{L}^{-1} \left\{ \frac{a}{s+a} \hat{v}_T(s) \right\} = v_{C0} e^{-at} + v_{Cp}(t)$$

- Neglect initial voltage v_{C0} as $t \rightarrow \infty$

$$(3.2.1-2) \quad v_C(t) = \mathcal{L}^{-1} \left\{ \frac{a}{s+a} \hat{v}_T(s) \right\} = v_{Cp}(t)$$

Since $a > 0$, $v_{C0} e^{-at}$ will vanish as $t \rightarrow \infty$, and then $v_C(t) = v_{Cp}(t)$ depends only on the source $v_T(t)$.

- Constant voltage source $v_T(t) = V_T$ or $\hat{v}_T(s) = \frac{V_T}{s}$

$$(3.2.1-3) \quad \hat{v}_C(s) = \frac{v_{C0}}{s+a} + \frac{a}{s+a} \hat{v}_T(s) = \frac{v_{C0} - V_T}{s+a} + \frac{V_T}{s}$$

$$\Rightarrow v_C(t) = (v_{C0} - V_T)e^{-at} + V_T = v_{C0}e^{-at} + V_T(1 - e^{-at})$$

As t increases, $v_{C0}e^{-at}$ is gradually ignorable and finally $v_C(\infty) = V_T$ depends only on the source V_T .

- Sinusoidal voltage source $v_T(t) = \cos \omega t$ or $\hat{v}_T(s) = \frac{s}{s^2 + \omega^2}$

$$(3.2.1-4) \quad \hat{v}_C(s) = \frac{v_{C0}}{s+a} + \frac{a}{s+a} \hat{v}_T(s) = \frac{v_{C0}}{s+a} + \frac{as}{(s+a)(s^2 + \omega^2)}$$

It can be obtained that

$$(3.2.1-5) \quad \frac{as}{(s+a)(s^2 + \omega^2)} = \frac{\alpha}{s+a} + \frac{\beta s + \lambda \omega}{s^2 + \omega^2}$$

$$= \frac{(\alpha + \beta)s^2 + (\lambda \omega + a\beta)s + a\lambda \omega + \alpha \omega^2}{(s+a)(s^2 + \omega^2)}$$

$$\Rightarrow \alpha + \beta = 0, \quad \lambda \omega + a\beta = a, \quad a\lambda \omega + \alpha \omega^2 = 0$$

$$\Rightarrow \alpha = -\frac{1}{1 + (R_T C \omega)^2}, \quad \beta = \frac{1}{1 + (R_T C \omega)^2}, \quad \lambda = \frac{R_T C \omega}{1 + (R_T C \omega)^2}$$

Hence, $\hat{v}_C(s) = \frac{v_{C0} + \alpha}{s+a} + \frac{\beta s + \lambda \omega}{s^2 + \omega^2}$, i.e.,

$$(3.2.1-6) \quad v_C(t) = (v_{C0} + \alpha)e^{-at} + \beta \cos \omega t + \lambda \sin \omega t$$

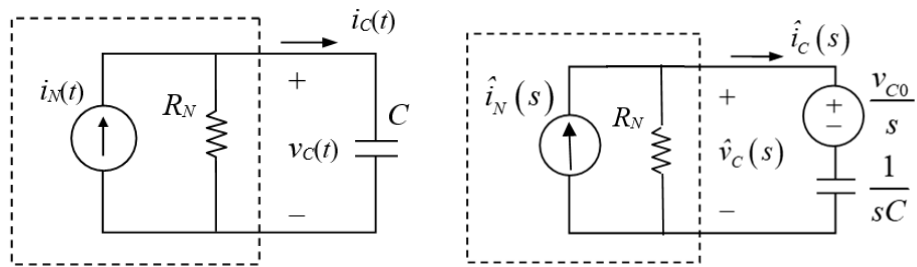
- As t increases, we have

$$(3.2.1-7) \quad v_C(t) = \beta \cos \omega t + \lambda \sin \omega t = \sqrt{\beta^2 + \lambda^2} \cos(\omega t + \theta) = A \cos(\omega t + \theta)$$

where $A = \frac{1}{\sqrt{1 + (R_T C \omega)^2}} < 1$ and $\theta = -\tan^{-1}\left(\frac{\lambda}{\beta}\right) = -\tan^{-1}(R_T C \omega) < 0$.

- A sinusoidal source $v_T(t) = \cos \omega t$ results in $v_C(t) = A \cos(\omega t + \theta)$, which is possessed of the same frequency ω , but with smaller magnitude $A < 1$ and delay phase $\theta < 0$.

3.2.2 RC Circuit with Current Source



- Mathematic model

$$(3.2.2-1) \quad i_N(t) = \frac{v_C(t)}{R_N} + i_C(t) = \frac{v_C(t)}{R_N} + C v_C'(t)$$

$$\Rightarrow v_C'(t) + \frac{1}{R_N C} v_C(t) = \frac{1}{C} i_N(t), \quad v_C(0) = v_{C0}$$

Taking Laplace transform results in

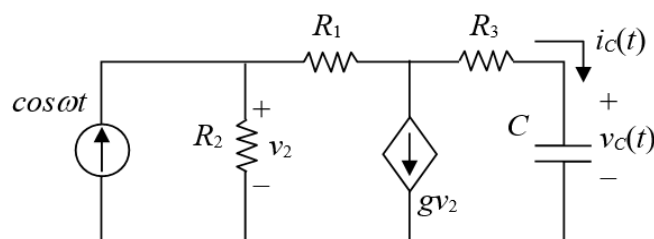
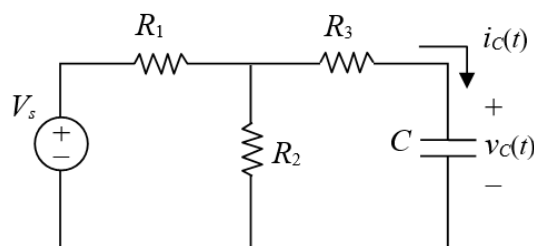
$$(3.2.2-2) \quad s \hat{v}_C(s) - v_{C0} + \frac{1}{R_N C} \hat{v}_C(s) = \frac{1}{C} \hat{i}_N(s)$$

$$\Rightarrow (s+b) \hat{v}_C(s) = b R_N \hat{i}_N(s) + v_{C0} \quad \left(b = \frac{1}{R_N C} \right)$$

$$\Rightarrow \hat{v}_C(s) = \frac{b R_N}{s+b} \hat{i}_N(s) + \frac{v_{C0}}{s+b}$$

$$\Rightarrow v_C(t) = \mathcal{L}^{-1} \left\{ \frac{b R_N}{s+b} \hat{i}_N(s) \right\} + v_{C0} e^{-bt}$$

Example: Determine $v_C(t)$.



3.3 RL Circuit

- Inductor model with initial current $i_L(0) = i_{L0}$

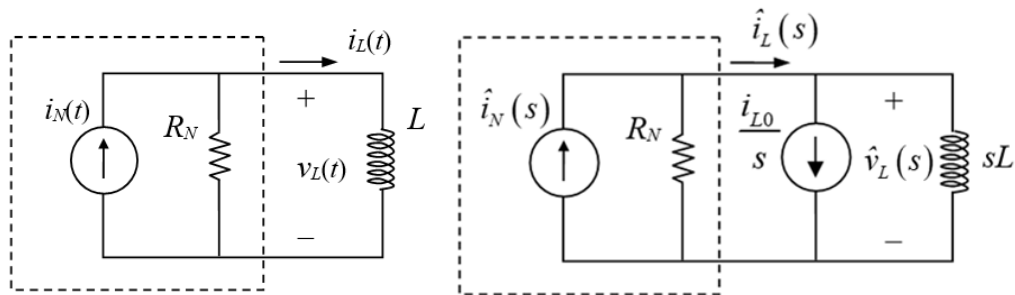
$$(3.3-1) \quad i_L(t) = i_{L0} + \frac{1}{L} \int_0^t v_L(\tau) d\tau$$

$$(3.3-2) \quad \hat{i}_L(s) = \frac{i_{L0}}{s} + \frac{1}{L} \left(\frac{\hat{v}_L(s)}{s} \right) \Rightarrow \hat{i}_L(s) = \frac{i_{L0}}{s} + \frac{1}{sL} \hat{v}_L(s)$$

$$z_L^{-1}(s)$$

$z_L(s) = sL$: impedance of inductor

3.3.1 RL Circuit with Current Source



- Mathematic model

$$(3.3.1-1) \quad \hat{i}_N(s) = \frac{\hat{v}_L(s)}{R_N} + \frac{i_{L0}}{s} + \frac{\hat{v}_L(s)}{sL} = \left(\frac{1}{R_N} + \frac{1}{sL} \right) \hat{v}_L(s) + \frac{i_{L0}}{s}$$

$$\Rightarrow \hat{v}_L(s) = \left(\frac{1}{R_N} + \frac{1}{sL} \right)^{-1} \left(\hat{i}_N(s) - \frac{i_{L0}}{s} \right) = \frac{sR_N L}{R_N + sL} \hat{i}_N(s) - \frac{R_N L i_{L0}}{R_N + sL}$$

$$\Rightarrow \hat{i}_L(s) = \frac{i_{L0}}{s} + \frac{1}{sL} \hat{v}_L(s) = \frac{i_{L0}}{s+a} + \frac{a}{s+a} \hat{i}_N(s), \quad a = \frac{R_N}{L}$$

$$\Rightarrow i_L(t) = \mathcal{L}^{-1} \left\{ \frac{i_{L0}}{s+a} \right\} + \mathcal{L}^{-1} \left\{ \frac{a}{s+a} \hat{i}_N(s) \right\} = i_{L0} e^{-at} + i_{Lp}(t)$$

- Neglect initial current i_{L0} as $t \rightarrow \infty$

$$(3.3.1-2) \quad i_L(t) = \mathcal{L}^{-1} \left\{ \frac{a}{s+a} \hat{i}_N(s) \right\} = i_{Lp}(t)$$

Since $a > 0$, $i_{L0} e^{-at}$ will vanish as $t \rightarrow \infty$, and then $i_L(t) = i_{Lp}(t)$ depends only on the source $v_T(t)$.

- Constant current source $i_N(t) = I_N$ or $\hat{i}_N(s) = \frac{I_N}{s}$

$$(3.3.1-3) \quad \hat{i}_L(s) = \frac{i_{L0}}{s+a} + \frac{a}{s+a} \hat{i}_N(s) = \frac{i_{L0} - I_N}{s+a} + \frac{I_N}{s}$$

$$\Rightarrow i_L(t) = (i_{L0} - I_N)e^{-at} + I_N = i_{L0}e^{-at} + I_N(1 - e^{-at})$$

As t increases, $i_{L0}e^{-at}$ is gradually ignorable and finally $i_L(\infty) = I_N$ depends only on the source I_N

- Sinusoidal voltage source $i_N(t) = \sin \omega t$ or $\hat{i}_N(s) = \frac{\omega}{s^2 + \omega^2}$

$$(3.3.1-4) \quad \hat{i}_L(s) = \frac{i_{L0}}{s+a} + \frac{a}{s+a} \hat{i}_N(s) = \frac{i_{L0}}{s+a} + \frac{a\omega}{(s+a)(s^2 + \omega^2)}$$

It can be obtained that

$$(3.3.1-5) \quad \frac{a\omega}{(s+a)(s^2 + \omega^2)} = \frac{\alpha}{s+a} + \frac{\beta s + \lambda \omega}{s^2 + \omega^2}$$

$$= \frac{(\alpha + \beta)s^2 + (\lambda\omega + a\beta)s + a\lambda\omega + \alpha\omega^2}{(s+a)(s^2 + \omega^2)}$$

$$\Rightarrow \alpha + \beta = 0, \lambda\omega + a\beta = 0, a\lambda\omega + \alpha\omega^2 = a\omega$$

$$\Rightarrow \alpha = \frac{L\omega/R_N}{1 + (L\omega/R_N)^2}, \beta = -\frac{L\omega/R_N}{1 + (L\omega/R_N)^2}, \lambda = \frac{1}{1 + (L\omega/R_N)^2}.$$

Hence, $\hat{i}_L(s) = \frac{i_{L0} + \alpha}{s+a} + \frac{\beta s + \lambda \omega}{s^2 + \omega^2}$, i.e.,

$$(3.3.1-6) \quad i_L(t) = (i_{L0} + \alpha)e^{-at} + \beta \cos \omega t + \lambda \sin \omega t$$

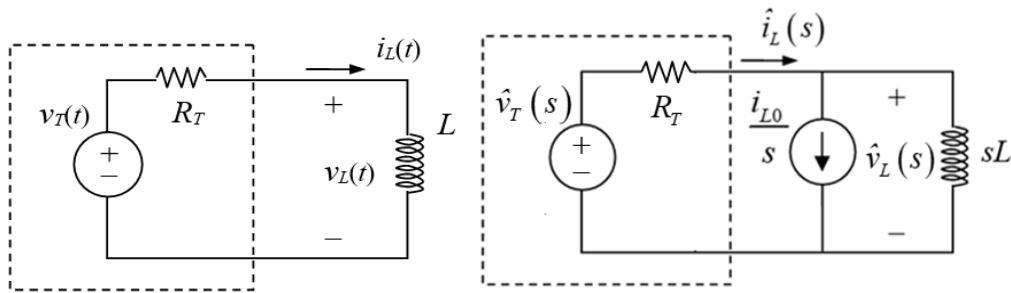
- As t increases, we have

$$(3.3.1-7) \quad i_L(t) = \beta \cos \omega t + \lambda \sin \omega t = \sqrt{\beta^2 + \lambda^2} \sin(\omega t + \theta) = A \sin(\omega t + \theta)$$

where $A = \frac{1}{\sqrt{1 + (L\omega/R_N)^2}} < 1$ and $\theta = \tan^{-1}\left(\frac{\beta}{\lambda}\right) = -\tan^{-1}(L\omega/R_N) < 0$.

- A sinusoidal source $i_N(t) = \sin \omega t$ results in $i_L(t) = A \sin(\omega t + \theta)$, which is possessed of the same frequency ω , but with smaller magnitude $A < 1$ and delay phase $\theta < 0$.

3.3.2 RL Circuit with Voltage Source



- Mathematic model

$$(3.3.2-1) \quad v_T(t) = R_T i_L(t) + v_L(t) = R_T i_L(t) + L i_L'(t)$$

$$\Rightarrow i_L'(t) + \frac{R_T}{L} i_L(t) = \frac{1}{L} v_T(t), \quad i_L(0) = i_{L0}$$

Taking Laplace transform results in

$$(3.3.2-2) \quad s \hat{i}_L(s) - i_{L0} + \frac{R_T}{L} \hat{i}_L(s) = \frac{1}{L} \hat{v}_T(s)$$

$$\Rightarrow (s + b) \hat{i}_L(s) = \frac{1}{L} \hat{v}_T(s) + i_{L0} = \frac{b}{R_T} \hat{v}_T(s) + i_{L0} \quad \left(b = \frac{R_T}{L} \right)$$

$$\Rightarrow \hat{i}_L(s) = \frac{b/R_T}{s + b} \hat{v}_T(s) + \frac{i_{L0}}{s + b}$$

$$\Rightarrow i_L(t) = \mathcal{L}^{-1} \left\{ \frac{b/R_T}{s + b} \hat{v}_T(s) \right\} + i_{L0} e^{-bt}$$

Example: Determine $i_L(t)$.

